

Optickle

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Abstract

Optickle is a general model for the electro-opto-mechanical part of an interferometric GW detector. It ventures into mechanics only as far as is necessary to include radiation pressure effects, and into electronics only far enough to produce demodulation signals, and into optics only up to first order. There are many other tools that do all these things in greater detail. Optickle is for quick, rough, but essentially complete interferometer design studies.

1 Introduction

As discussed in previous sections (to be written), Optickle can, in principal, simulate any interferometer. Once the construction of an Optickle model is finished, all the optics, links and probes added and happily in place, nothing useful has yet been done. At some point the information represented by the Optickle model must be converted into field amplitudes, and transfer functions. This document will discuss the theory and implementations of the functions which perform this conversion.

2 Example System

In the following sections, I will make frequent attempts to clarify by reference to the example optical system presented in this section. The example is a Fabry-Perot cavity, composed of two mirrors a source (the laser) and a sink (the photo-detector, see figure 1).

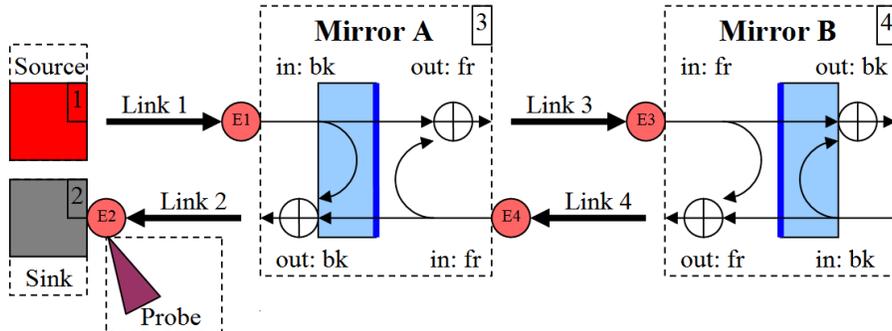


Figure 1: The example system: a Fabry-Perot cavity.

The source is responsible for illuminating the system. Let's assume that it generates a carrier and 2 RF sidebands from RF phase modulation approximated to first order. Thus, the frequencies of the field components, relative to the carrier field, are $\vec{v}_{f_{RF}} = [-f_{mod}, 0, f_{mod}]$, where f_{mod} is the RF modulation frequency.

The field produced by the source propagates via Link 1 to the back input of Mirror A. At the end of each link is a "field evaluation point", or FEP. FEPs are represented by light red balls in figure 1, and are labeled E1, E2, etc. The field at E1, for example, is clearly just the source field multiplied by the propagation phase determined by the length of Link 1.

The field computation can be described in two parts: static (DC) fields, and audio frequency (AF) fields. The DC fields are present in the optical system when none of the optics are driven. The AF fields are the fields generated by driving the optics. The following sections describe these computations in detail.

3 DC Fields

The collection of DC fields is relatively small: one for each RF field component, at each field evaluation point (FEP). That is, $N_{field} = N_{RF}N_{link}$, where N_{RF} is the number of RF components and N_{link} the number of links, such that for our example system $N_{RF} = 3, N_{link} = 4 \Rightarrow N_{field} = 12$. Despite this not being a very big number, it is enough to make matrices unwieldy and complicated, so for the next few paragraphs I'll use $\vec{v}_{f_{RF}} = [f_{mod}]$. To compute the DC fields in

the optical system Optickle assumes the steady state equation

$$\vec{v}_{DC} = \mathbf{M}_{DC}\vec{v}_{DC} + \vec{v}_{source} \quad (1)$$

where \mathbf{M}_{DC} is the optical propagation matrix between FEPs, \vec{v}_{DC} is the vector of fields at each FEP, and \vec{v}_{source} is the vector of injected fields (e.g., from the source in figure 1). Solving for \vec{v}_{DC}

$$\vec{v}_{DC} = (\mathbb{I} - \mathbf{M}_{DC})^{-1}\vec{v}_{source} \quad (2)$$

where \mathbb{I} is the identity matrix. The sources are given, so \vec{v}_{source} is known and the computation boils down to computing the inverse of $\mathbb{I} - \mathbf{M}_{DC}$. The propagation matrix is built from the optics and links in the optical system. For example, the matrix element which takes E4 to E3 is determined by the reflectivity of Mirror A and the length of Link 3. Thus, this element¹ of \mathbf{M}_{DC} is

$$\mathbf{M}_{DC}(3, 4) = -r_A e^{i2\pi f_{mod} l_3/c}. \quad (3)$$

More generally speaking, \mathbf{M}_{DC} is the sum of all of the input to output transfer matrices of all optics, multiplied by the phase induced by the links,

$$\mathbf{M}_{DC} = \mathbf{M}_\phi \mathbf{M}_{opt} \quad (4)$$

with

$$\mathbf{M}_{opt} = \sum_{n=1}^{N_{optic}} \mathbf{M}_{out_n} \mathbf{M}_{opt_n} \mathbf{M}_{in_n}. \quad (5)$$

As shown in the above equation, the contribution of a given optic to the overall transfer matrix is made up of three parts, a matrix which maps FEPs onto the inputs of the optic, the optic's own transfer matrix, and a matrix which maps the optic's outputs back to FEPs.

Taking Mirror A again from our example system (figure 1), and noting that its index is 3, its front input is from FEP 4 and its back input from FEP 1, the corresponding input matrix is

$$\mathbf{M}_{in_3} = \begin{bmatrix} 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \end{bmatrix}.$$

¹The indexing used in this document will reflect what is used in the Optickle code. Indices will start at 1, and the colon operator indicates a series of integers (both standard in Matlab).

where a given excitation vector produces a vector of audio sideband fields. A further transformation, determined by the probes place in the system, converts fields to signals

$$\vec{v}_{signal} = \mathbf{M}_{prb}(\mathbb{I} - \mathbf{M}_{AC})^{-1}\vec{v}_{excitation} \quad (9)$$

The transfer matrix, from normalized excitations to signals, is thus just the core of the above equation,

$$\mathbf{M}_{TF} = \mathbf{M}_{prb}(\mathbb{I} - \mathbf{M}_{AC})^{-1}. \quad (10)$$

This matrix is one of the primary results produced by the Optickle compute function.

In Optickle the audio frequency transfer matrix, \mathbf{M}_{AC} , is constructed in blocks

$$\mathbf{M}_{AC} = \begin{bmatrix} \mathbf{M}_{field-field} & \mathbf{M}_{optic-field} \\ \mathbf{M}_{field-optic} & 0 \end{bmatrix}. \quad (11)$$

where $\mathbf{M}_{field-field}$ is a matrix similar to \mathbf{M}_{DC} which represents transfers among fields, though in this case they are AF sideband fields. The $\mathbf{M}_{optic-optic}$ matrix is missing as the optics' degrees of freedom are assumed to be decoupled. As the names indicate, $\mathbf{M}_{optic-field}$ and $\mathbf{M}_{field-optic}$ represent the relationships between the optics' degrees of freedom and the AF sideband fields. The following sections will describe the construction of each of these matrices in detail.

4.1 Field to Optic Transfer Matrix

This matrix is actually the product of the field-to-force matrix, and the force-to-degree of freedom matrix, where "degree of freedom" most often means "position".

$$\mathbf{M}_{field-optic} = \mathbf{M}_{rct}\mathbf{M}_{field-force} \quad (12)$$

To compute the force available for generating mechanical motion, we start with the force exerted on a perfect absorber

$$F_0 = (E_{DC}^*E_- + E_{DC}E_+^*)e^{-i2\pi f_{AF}t}/c, \quad (13)$$

where the audio frequency phase rotation part has been factored out of the audio sideband amplitudes, E_- and E_+ , and the DC and AF

fields are both associated with the same RF component. A not normally noteworthy feature of equation 13 is that the upper audio sideband appears conjugated. This has implications for the matrix world of Optickle, since matrices do not usually contain conjugation operators. To side-step this problem, the conjugate of the upper sideband is propagated throughout the system with appropriately conjugated operators.

The reaction matrix \mathbf{M}_{rct} is typically the mechanical response of the optics to radiation pressure induced force, summed over all optics in the system,

$$\mathbf{M}_{rct} = \sum_{n=1}^{N_{optic}} \mathbf{M}_{DOF_n} \mathbf{M}_{rct_n} \mathbf{M}_{in_n} \quad (14)$$

where \mathbf{M}_{DOF_n} is the matrix which maps the internal degrees of freedom of the n^{th} optic onto the system wide degrees of freedom. $\mathbf{M}_{field-force}$ comes directly from equation 13,

$$\mathbf{M}_{field-force} = \left[\text{diag}(\vec{v}_{DC})^* \quad \text{diag}(\vec{v}_{DC}) \right] / c \quad (15)$$

where “diag” is Matlab notation for “a square matrix with this vector along the diagonal.”

Expanding our discussion to TEM01 and 10 modes would lead us to consider the field-to-torque and torque-to-angle matrices, but we can save that for later.

4.2 Field to Field Transfer Matrix

This part of is almost identical to \mathbf{M}_{DC} , the major differences being that for each RF component 2 AF sidebands must be computed, and that the propagation phase associated with the links must account for the sum of the RF and AF phases. Restating,

$$\mathbf{M}_{field-field} = \left[\begin{array}{cc} \mathbf{M}_{\phi_-} \mathbf{M}_{opt} & 0 \\ 0 & \mathbf{M}_{\phi_+}^* \mathbf{M}_{opt}^* \end{array} \right] \quad (16)$$

where in this case the link phase is

$$\mathbf{M}_{\phi_{\pm}}(k, k) = e^{i (\vec{v}_{fRF}(m) \pm f_{AF}) \vec{v}_{length}(n)} \quad (17)$$

which is the same as equation 6, with the addition of the audio frequency component. The conjugation of the upper sideband component is a result of equation 13, as mentioned earlier.

4.3 Optic to Field Transfer Matrix

The optic to field matrix, much like the field to field matrix, must result in both upper and lower audio sidebands at FEPs, so it is constructed as

$$\mathbf{M}_{optic-field} = \begin{bmatrix} \mathbf{M}_{\phi_-} \mathbf{M}_{gen} \\ \mathbf{M}_{\phi_+}^* \mathbf{M}_{gen}^* \end{bmatrix} \quad (18)$$

The matrix \mathbf{M}_{gen} is composed of an optic specified matrix and DC fields. The DC fields are present as source fields which the optics modulate to produce audio SBs,

$$\mathbf{M}_{gen}(:, k_{n,m}) = \mathbf{M}_{drv_{n,m}} \vec{v}_{DC} \quad (19)$$

where $\mathbf{M}_{drv_{n,m}}$ is the modulation produced by driving optic n , degree of freedom m . The indices are $n \in 1 : N_{optic}$, $m \in 1 : N_{dof_n}$, and $k_{n,m}$ is the map of system degrees of freedom to optics internal degrees of freedom. $k_{n,m}$ is related to \mathbf{M}_{DOF_n} from equation 14 by

$$\mathbf{M}_{DOF_n}(k_{n,m}, m) = 1 \quad (20)$$

with all other elements of $\mathbf{M}_{DOF_n} = 0$. This mapping is a bit ugly, but it can only be avoided by using higher dimensional tensors, which seem even less appealing.

The drive matrix $\mathbf{M}_{drv_{n,m}}$ can be written in terms of \mathbf{M}_{opt_n}

$$\mathbf{M}_{drv_{n,m}} = \mathbf{M}_{out_n} \frac{1}{2} \frac{\partial \mathbf{M}_{opt_n}}{\partial x_{n,m}} \mathbf{M}_{in_n} \quad (21)$$

where $x_{n,m}$ the m^{th} degree of freedom of the n^{th} optic. The usual input and output transforms are in place to map the source fields in and the generated audio-sidebands out. After the output mapping, \mathbf{M}_{ϕ} appears in equation 18 to carry the audio-sidebands from the output of the optics where they are generated, which are inputs of the associated links, to the FEPs at the outputs of the links.

5 Signal Production

Converting DC and audio frequency fields to signals is the job of probes place in the system. Probe signals result from power measured by the probe and is thus similar to the radiation pressure interaction described in $\mathbf{M}_{field-optic}$. The major difference is that probes can demodulate signals at RF frequencies, thereby mixing RF components.

As with fields, there are two computations to perform: DC and AC. DC signals are the signals present given only the DC fields present, and are thus related to the current working point of the Optickle system. AC signals, on the other hand, are products between DC and audio frequency fields: they tell us about the response of the system around the current working point as seen in equation 9.

5.1 DC Signals

To compute the DC signals, we start with an expression for the intensity present at a given FEP,

$$I = \sum_{m=1}^{N_{RF}} \sum_{n=1}^{N_{RF}} E_{DC_n}^* E_{DC_m} e^{i2\pi(\vec{v}_{f_{RF}}(m) - \vec{v}_{f_{RF}}(n))t} \quad (22)$$

where E_{DC_n} is the field amplitude of the n^{th} RF component, with the RF phase rotation factored out (much like equation 13 for field induced forces).

Requiring that the output be at the demodulation frequency f_{demod} , such that the integral

$$S_{DC} = \int_{-\infty}^{\infty} I \cos(2\pi f_{demod}t + \phi_{demod}) dt \quad (23)$$

is non-zero removes most of the terms in the sum by introducing a delta function

$$S_{DC} = \sum_{m=1}^{N_{RF}} \sum_{n=1}^{N_{RF}} E_{DC_n}^* E_{DC_m} \delta_{n,m} \quad (24)$$

where

$$\delta_{n,m} = \delta(\vec{v}_{f_{RF}}(m) - \vec{v}_{f_{RF}}(n) + f_{demod}) e^{i\phi_{demod}} + \delta(\vec{v}_{f_{RF}}(m) - \vec{v}_{f_{RF}}(n) - f_{demod}) e^{-i\phi_{demod}}.$$

Translating this into the language of matrix manipulation, the DC signal from the k^{th} probe is

$$\vec{v}_{sig_{DC}}(k) = (\mathbf{M}_{prb_k} \mathbf{M}_{pin_k} \vec{v}_{DC}^*)^T \mathbf{M}_{pin_k} \vec{v}_{DC}, \quad (25)$$

where the probe's matrix expresses the delta function in equation 24 as the matrix

$$\mathbf{M}_{prb_k}(m, n) = \delta_{n,m}, \quad (26)$$

and \mathbf{M}_{pin_k} is the input map for the probe.

5.2 AC Signals

AC signal computation follows a very similar path. The audio frequency signal present at a given FEP is

$$S_{AC} = \sum_{m=1}^{N_{RF}} \sum_{n=1}^{N_{RF}} (E_{DC_n}^* E_{-m} \delta_{n,m} + E_{DC_n} E_{+m}^* \delta_{m,n}). \quad (27)$$

The overall probe matrix is constructed from the individuals row at a time according to

$$\mathbf{M}_{prb}(k, :) = \left[\begin{array}{c} \mathbf{M}_{prb_k} \mathbf{M}_{pin_k} \vec{v}_{DC}^* \\ \mathbf{M}_{prb_k}^T \mathbf{M}_{pin_k} \vec{v}_{DC} \end{array} \right]^T \left[\begin{array}{c} \mathbf{M}_{pin_k} \\ \mathbf{M}_{pin_k} \end{array} \right], \quad (28)$$

where $k \in 1 : N_{probe}$. Note that the probe matrix \mathbf{M}_{prb_k} for the upper audio sideband is the transpose of that for the lower sideband, as m and n are exchanged for the upper sideband in equation 27. It may seem odd that the input map is used so many times: two instances are for the DC fields in \vec{v}_{DC} and \vec{v}_{DC}^* , other two bring in the correct the upper and lower audio frequency fields from \vec{v}_{AC} which is expected to arrive on the right (see equations 8 and 9).

6 Quantum Noise

This section is still under construction!

Computed by injecting AF SB at each loss point, unconnected port, and source. This is implemented, but not yet documented.

7 Angular Transfer Functions

This section is still under construction!

Optickle can compute transfer functions for the TEM01 mode produced, for example, by pitch of a mirror. This is done in almost complete analogy with the TEM00 computations described in the previous sections. The exceptions are the Gouy phase, and the dependence of audio sideband injection amplitude on the Hermite-Gaussian beam parameters.

Examples: mirror onto diode 1m away, FP in cavity and on transmission with Gouy telescope, etc.

8 Parting Example

This section is still under construction!

A quick example of how to run the compute function and how to interpret its results would be good.